2. Dada la viga simplemente apoyada de momento de inercia Nonable, determine el giro y la flecha en el punto de la carga aplicada por el momento de doble integración. Se conoce $I_1 = 16650 \text{ cm}^4$ $I_2 = 12500 \text{ cm}^4$. $E = 2 \times 10^8 \text{ kg/cm}^2$

20TN

20(270) = 450 RB

12TN = RB

12TN = RB

8TN = RA

270cm

180cm

$$R_{B}$$

0<7 < 180

ET; Y_{1}^{1} = RAX

ET; Y_{2}^{1} = RB Z

ET; Y_{1}^{1} = RAX² + C1

ET; Y_{1}^{1} = RAX³ + C1X + C2

Fara X=0 Y₁ = 0 Q=0

Para Z=0 Y₂ = 0 C4 = 0

1EVA

CONDICION FOONTERA Y'_{1} = -Y'_{2} X = 270 Z = 180

$$\frac{1}{2} (\frac{RAX^{2}}{2} + C_{1}) = \frac{1}{ET_{2}} (\frac{REZ^{2}}{2} + C_{3})$$

$$\frac{2916 \times 10^{5} \text{ Kgxcm}^{2}}{2} + \frac{C_{1}}{2} = \frac{1944 \times 10^{5} \text{ Kgxcm}}{2 \times 10^{5} \text{ Kgxcm}} + \frac{C_{3}}{2 \times 10^{5} \text{ Kgxcm}}$$

 $2916 \times 10^{5} + \hat{c}_{1} = \frac{T_{1}}{T_{2}} \left[1944 \times 10^{5} + \epsilon_{3} \right]$

 $291600000 + C_1 = -[258940800 + 1.332C_3]$

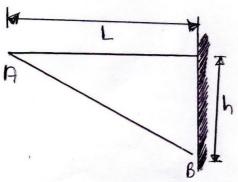
550540800 401 + 1.33203 = 0

 $2^{04} \text{ condicion Frontera} \quad y_1 = y_2 = 7 \quad x = 270 \quad z = 180 \qquad C_1 = -2440 \underline{10880}$ $\frac{1}{ET_1} \left[\frac{RAx^3 + C_1 x}{6} \right] = \frac{1}{ET_2} \left[\frac{RBz^3 + C_3 z}{6} \right] \quad C_2 = -230127567.6$ $2.6244 x 10 + 270 c_1 = \frac{T_1}{T_2} \left[1.1664 x 10 + 180 G \right]$

1.0707552 x10 + 270 C1 - 239,76 C3 =0

 $y'_{i} = 1.429702703 \times 10^{-3}$ $y'_{i} = -1.190358$ cm PPTA

Determinar la deflexión en el punto "A" de la viga que se representa en la figura, debido a su peso propio se sabe que el peso específica del material de la viga es "X", el modulo de elastiadad "E" y el anch de la viga es "b"



$$IEy'' = -\frac{8hb}{2L}x^2(\frac{x}{3}) = -\frac{8hb}{6L}x^3$$

$$EV'' = \frac{-\frac{3hb}{6L}x^3}{\frac{bh^3}{12L^3}x^3} = -\frac{28L^2}{h^2}$$

$$f A_1 = -\frac{\mu_S}{5 R \Gamma_S} \times + c^4$$

$$Ey = -2 \frac{x^2}{h^2} \frac{x^2}{x^2} + c_1 x + c_2$$

Sara
$$x=L y=0 c_1 = \frac{28L^3}{N^2}$$

Para
$$x=L$$
 $y=0$ $c_2=-\frac{\partial L^4}{h^2}$

$$EY = -\frac{8L^4}{n^2}$$

$$y_A = -\frac{8L^4}{Eh^2}$$
 RPTA

$$h(x) = h$$

$$h(x) = h$$

$$h(x) = h \times 1$$

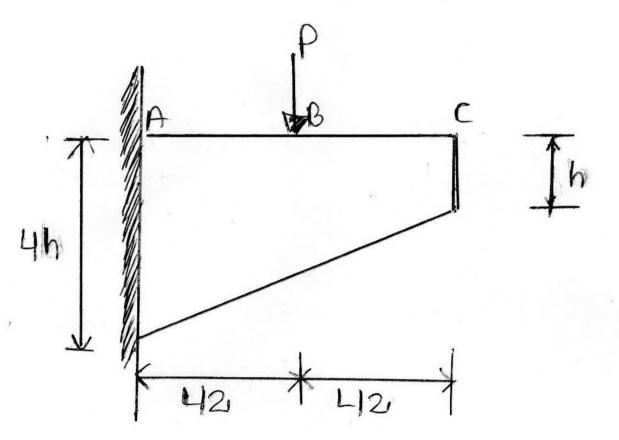
$$h(x) = h \times 2$$

$$V = \frac{1}{2}h(x)bx = \frac{hb}{2L}x^{2}$$

$$W = \frac{3^{1}hb}{2L}x^{2}$$

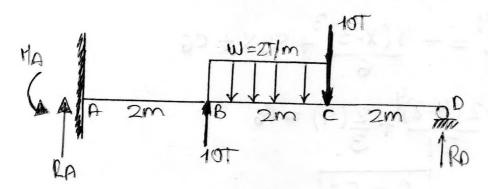
$$T = b(hx)^{3} = \frac{bh^{3}}{12L^{3}}x^{3}$$

La viga mostrada de sección variable es de un solo material con módulo de elasticidad E coluitar la deflexión en el punt de aplicación de la carga P.



doble integración

Resolver la viga y déterminar el volter de la déflexión múxima aplicando el método de la doble integración. El = de



Tramo
$$0 \le x \le 2$$

I, $= y''_1 = RAx - M$
 $= RAx^2 - Mx + A$
 $= RAx^3 - Mx^2 + 4x^2 + 4x^3$

Sara
$$x=0$$
 $y'_1=0$ $c_1=0$

Sara $x=0$ $y'_1=0$ $c_2=0$

Sara $y'=0$ $x=0$

Tramo 2 < x < 4

$$IEY_{2}^{"} = RAX - M + 10(X-2) - \omega(X-2)^{2} \quad \text{fora } X=2 \quad y_{1}=y_{2} - D \quad C_{3}=0$$

$$IEY_{2}^{"} = RAX^{2} - MX + 10(X-2)^{2} - \omega(X-2)^{2} + C_{3} \quad \text{fora } X=2 \quad y_{1}=y_{2} - D \quad C_{4}=0$$

$$IEY_{2} = \frac{RAX^{2}}{2} - \frac{MX}{2} + \frac{10(X-2)^{2}}{6} - \frac{\omega(X-2)^{2}}{6} + \frac{10(X-2)^{2}}{24} + \frac{10(X-$$

tramo 4 & x < 6

$$IEY_3'' = RAX - H + 10(X-2) - 4(X-3) - 10(X-4)$$

$$IEY_3' = \frac{RAX^2 - HX + 10(X_1^2)^2 - 4(X_2^{-3})^2 - 10(X_2^4)^2 + C_5}{2}$$

$$IEY_3 = \frac{RAX^2 - HX + 10(X_1^2)^2 - 4(X_2^{-3})^2 - 10(X_2^4)^3 + C_5X + C_6}{6}$$

Pora
$$x=4$$
 $y_2=y_3'$
 $-\omega \left(\frac{4-2}{6}\right)^3 = -4\left(\frac{x-3}{2}\right)^2 + c_5$

$$\frac{4(1)^{2}-2(2)^{3}=5}{2}$$

Sara
$$x=4$$
 $y_1=y_2$

$$-\frac{w(x-2)^4}{24} = -\frac{4(x-3)^3}{6} + \frac{c_5x + c_6}{6}$$

$$\frac{4(4-3)^3 - 2(4-2)^4 + 2(4) = c_6}{24}$$

$$2 = c_6$$

Para
$$x=6m$$
 $y_2=0$

$$0 = \frac{RA(6)^3}{6} - \frac{M(6)^2}{2} + \frac{10}{6}(4)^3 - \frac{4(3)^3}{6} - \frac{10}{6}(2)^3 - \frac{2}{3}(6) + \frac{10}{3}(6) + \frac{1$$

$$0 = 36RA - M_A + \frac{220}{3}$$

$$6RA + 10(4) - 4(3) - 10(2) - MA = 0$$

$$RA = \frac{-53}{54} TN$$
 $H = \frac{19}{9} TN \times m$ $RD = \frac{269}{54} TN$

La viga paraalmente en voladizo de acero ABC soporta una carga concentrada P en el extremo c. para la porción AB de la viga:

- a) obtenga la euración de la curva elástica
- b) determine la deflexión máxima

IEY =
$$RAX$$

IEY = $RAX^2/2 + C_1$

IEY = $RAX^3/6 + C_1X + C_2$

$$I = y_2^{11} = RAX + RB(X-L)$$

$$I = y_2^{1} = RAX^{2}/2 + RB(X-L)^{2}/2 + C_3$$

$$I = y_2 = RAX^{3}/6 + RB(X-L)^{3}/6 + C_3X + C_4$$

RB.L = P(L+a)

 $RA = \frac{Pq}{r} (1)$

 $RB = \frac{P}{\Gamma}(L+a)(\uparrow)$

Sara
$$x=0$$
 $C_2=0$
Sara $x=L$ $y_1=y_2=0$ $c_1=c_3$
 $0=-\frac{Pa(L^3)}{6L}+c_1L$ $n=\frac{PaL}{6}$

(1)
$$IEY_1 = -\frac{Pa}{6}x^3 + \frac{Pal}{6}x$$

b) deflexión máxima -> grro = 0

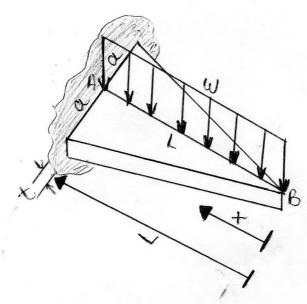
$$0 = -\frac{\rho_0}{2L} x^2 + \frac{\rho_0 L}{6} \implies \frac{\rho_0}{2L} x^2 = \frac{\rho_0 L}{6} \implies x^2 = \frac{L^2}{13^2}$$

$$x = 0.577L$$

$$00 \text{ TEY,} = -\frac{Pq}{6L} (0.577L)^3 + \frac{PqL}{6} 10.577L)$$

good injection and

La viga mostrada tiene un espesar constante "t", esta en nolodiza (empotramiento en "A") y es de un moterial de módulo «E". Determinor el nolor de la deflexión máximo



$$Ix = Y'' = -\frac{\omega x^2}{2}$$

$$EY'' = -\frac{\omega x^2}{2Ix} = -\frac{\omega x^2}{\frac{2}{2at^3x}} = -\frac{12\omega x^2}{4at^3x}$$

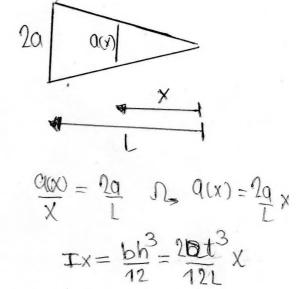
$$\sqrt{EY''} = -\frac{3\omega xL}{\cot^3}$$

$$\sqrt{EY} = -\frac{wx^3L+c_1x+c_2}{2at3}$$

$$C_1 = \frac{3wl^3}{2at^3}$$

$$c_2 = \frac{wt^4}{2at^3} - \frac{3wt^4}{2at^3}$$

$$\left\{c_{2} = \frac{-\omega L^{4}}{\omega t^{3}}\right\}$$



deflexion máxima dmax = db

$$EY = C_2$$

$$EY = -wL^4$$

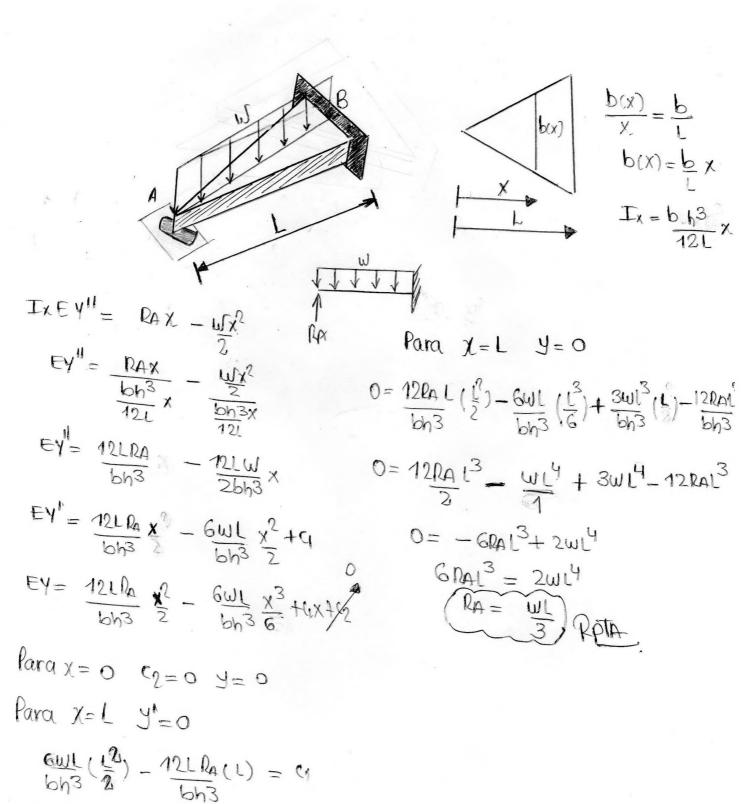
$$u = -wL^4$$

$$at3$$

$$U = -wL^4$$

$$Eat^3$$

La viga mostrada tiene un soporte senallo en A y un empotramiento en B. El momento de Inercias de las secuones transversoles novía linealmente desde cero en A a Io en B. Calcular la reacción en el soporte A debido a la cargo lineal uniforme de intensidad W.

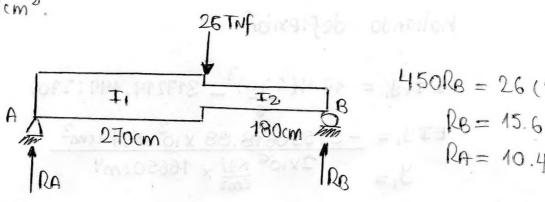


 $\frac{3WL^3}{bb^3} - \frac{12RAL^2}{113} = 0$

Dada la viga simplemente apoyada de momento de ineraca voriable, determine el giro y flecha en el punto de la carga aplicada por el método de la doble integración. Se conoce $I_1 = 16650$ cm⁴ $I_2 = 12500$ cm E = 2x10 Kf/cm2. 26 TNF 1891 Job Comment

450RB = 26 (270)

RA= 10.4



$$I_1 \in \mathcal{Y}_1^{11} = 10.4 \text{ x}^2/2 + C_1$$
 $I_2 \in \mathcal{Y}_2^{11} = 15.6 \text{ z}^2$
 $I_1 \in \mathcal{Y}_1^{12} = 10.4 \text{ x}^2/2 + C_1$
 $I_2 \in \mathcal{Y}_2^{12} = 15.6 \text{ z}^2/2 + C_3$
 $I_3 \in \mathcal{Y}_3^{12} = 10.4 \text{ x}^3/6 + C_3 \text{ z} + C_3$
 $I_4 \in \mathcal{Y}_2^{12} = 15.6 \text{ z}^3/6 + C_3 \text{ z} + C_3$

Para
$$x = 270 \, \text{cm}$$
 $z = 180 \, \text{cm}$ $y_1 = y_2$

$$10.4 \frac{x^{3}}{6} + 4x = \frac{I_{1}}{I_{2}} \left(15.6 \frac{z^{3}}{6} + 5.7 z \right)$$

$$10.4 \left(\frac{270}{6} \right)^{3} + 2700 = \frac{16650}{12500} \left(\frac{15.6}{6} \left(\frac{180}{6} \right)^{3} + 1800 \right)$$

Para
$$X = 270 \text{cm}$$
 $\Xi = 180 \text{cm}$ $Y_1' = -Y_2'$
 $10.4 \frac{\chi^2}{2} + C_1 = \frac{\Xi_1}{\Xi_2} \left(-15.6 \frac{\Xi^2}{2} + C_3 \right)$
 $10.4 \left(\frac{180^2}{2} + C_1 \right) = \frac{16650}{12500} \left(-15.6 \left(\frac{180}{2} \right)^2 - C_3 \right)$

$$C_1 + 1.332C_3 + 715703.04 = 0$$

hallando deflexión

EI,
$$y_1 = 10.4(270)^3 - 317214.144(270)$$

$$y_1 = -51530618.88 \times 10^3 \text{ Kgf} \times 10^3 \times$$

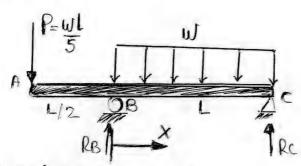
hallando giro

TO LYNE AL

$$y'_1 = \frac{61865.856 \times 10^3}{2 \times 10^6 \times 16650}$$

Para la inga y carga que se muestra en la figura en wentre:

- a) Ecuación de la curva elóstica para el tramo be de la viga
- b) deflexión en la mitad de la luz
- c) la pendiente en B



$$\frac{\text{wl}}{5} \left(\frac{3\text{L}}{2} \right) + \frac{\text{wl}^2}{2} = \text{RB(L)}$$

$$\text{RB} = \frac{4\text{wl}}{5}$$

$$\text{RA} = \frac{2\text{wl}}{5}$$

$$IEy'' = -\frac{WL}{5} \left(\frac{L}{2} + X \right) + \frac{4WLX}{5} - \frac{WX^2}{2}$$

$$TEY' = \frac{4}{5}\omega LX - \frac{\omega L^2}{10} - \frac{\omega LX}{5} - \frac{\omega x^2}{2}$$

$$TEY' = \frac{4\pi L}{10} x^2 - \frac{\pi L^2}{10} x - \frac{\pi L}{10} x^2 - \frac{\pi x^3}{6} + 0$$

TEY =
$$\frac{4wL}{30}x^3 - \frac{wl^2}{20}x^2 - \frac{wL}{30}x^3 - \frac{wx^4}{24} + 4x + 62$$

$$TEY = \frac{WL}{10} x^3 - \frac{Wl^2}{20} x^2 - \frac{W}{24} x^4 + c_1 x + c_2$$

Para
$$x=0$$
 $c_2=0$

Apra
$$x=0$$
 $y=0$

$$0 = \frac{\omega L}{10} (L^{3}) - \frac{\omega L^{2}}{20} (L^{2}) - \frac{\omega}{24} (L^{4}) + C_{1}(L)$$

$$C_{1} = \frac{-\omega L^{3}}{120}$$

$$C_{1} = \frac{-\omega L^{3}}{120}$$

$$C_1 = \frac{-\omega L^3}{120}$$
 Pola

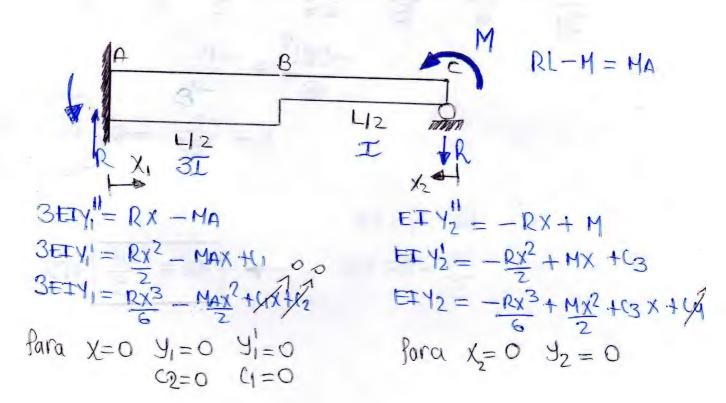
a)
$$\pm 4 = \frac{WL}{10} x^3 - \frac{W}{24} x^4 - \frac{Wl^2}{20} x^2 - \frac{Wl^3}{120} x$$

b)
$$\text{Tey} = \frac{\omega L}{10} \left(\frac{L}{2}\right)^3 - \frac{\omega}{24} \left(\frac{L}{2}\right)^4 - \frac{\omega L^2}{20} \left(\frac{L}{2}\right)^2 - \frac{\omega L^3}{120} \left(\frac{L}{2}\right) \mathcal{N}_{\bullet} = \frac{19\omega L^4}{1920 \text{ ET}}$$

TEO_B= CI
$$\Rightarrow$$
 OB = $\frac{-\omega L^3}{120EI}$ PPA

Pora la viga ABC mostroda en la figura 1, 5e conocen E, I, M, L Se pide determinar, utilizando el método de doble integración lo siguier

- a) El momento en el empotramiento A
- b) La rigidez ABSOLUTA de la riga ABC.



Para
$$X_{1}=1_{12}$$
 $X_{2}=1_{12}$ $Y_{1}=Y_{2}$

$$\frac{Rx^{3}-M_{4}x^{2}}{18}=\frac{-Rx^{3}+M_{2}x^{2}+C_{3}x}{6}$$

$$\frac{Rx^{3}-R_{1}x^{2}+M_{2}x^{2}+R_{2}x^{3}-M_{2}x^{2}=C_{3}x}{6}$$

$$\frac{Rx^{3}-R_{1}x^{2}+M_{2}x^{2}+R_{2}x^{3}-M_{2}x^{2}=C_{3}x}{6}$$

$$\frac{RI^{3}-R_{1}^{3}+R_{2}^{3}+R_{2}^{3}+M_{2}^{3}-M_{2}^{3}=C_{3}x}{6}$$

$$\frac{RI^{3}-R_{1}^{3}+R_{2}^{3}+R_{2}^{3}+R_{2}^{3}-R_{2}^{3}}{12}$$

$$\frac{RI^{3}-R_{1}^{3}+R_{2}^{3}+R_{2}^{3}-R_{2}^{3}-R_{2}^{3}}{12}$$

$$\frac{RI^{3}-R_{1}^{3}+R_{2}^{3}-R$$

$$-\frac{RL^{2}}{36} - \frac{ML}{6} = \frac{C_{3}}{6}$$

$$M = \frac{5RL}{9} - RL = \frac{9M}{5}$$

$$\frac{9M}{5} - M = MA$$

$$\frac{9M}{5} - M = MA$$

$$\frac{MA}{5} = \frac{4M}{5} \frac{RPTA}{5}$$

dople integracion

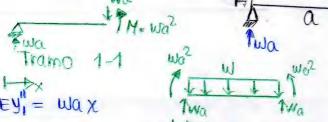
Por el métado de doble integración, de la viga mostrada, determinar:

W

1.5 I

- a) deflexion en el contro de luz de la viga
- b) Pendiente en A
- c) Pendiente en B
- d) OFC





$$TEY = Wax^2 + C_1$$
 0 1.5:

$$\pm 3 = \frac{2}{6}$$

TEY =
$$w_0 x^2 + c_1$$

TEY = $w_0 x^2 + c_1$

1.5 IEY = $w_0 x^3 + c_1 x + c_2$

1.5 IEY = $w_0 x^3 + c_1 x + c_2$

1.5 IEY = $w_0 x^3 + c_1 x + c_2$

1.5 IEY = $w_0 x^3 + c_1 x + c_2$

1.5 IEY = $w_0 x^3 + c_1 x + c_2$

$$1.5 \text{ IEy}_{2} = \frac{\sqrt{3}}{6} + \frac{\sqrt{3}}{2} \times \frac{\sqrt{3}}{6} + \frac{\sqrt{3}}{24} +$$

$$TEY'_3 = Wax$$

$$TEY'_2 = Wax^2 1 Ce$$

$$T = y_3 = w_{0x}^2 + c_5$$

$$T = y_3 = w_{0x}^3 + c_5x + c_6$$

• Para
$$x_1 = a$$
 $x_2 = 0$: $y_1 = y_2$ $y_1 = y_2'$

$$\frac{\text{Wa}}{6}(a^3) + \text{C1}(a) = \frac{2}{3}\text{C4}$$
 $A = \frac{\text{Wa}}{2}(a)^2 + \text{C1} = \frac{2}{3}\text{C3}$
 $A = \frac{\text{Wa}}{2}(a)^2 + \text{C1} = \frac{2}{3}\text{C3}$

$$\frac{wa^{4} + c_{1}q = \frac{2}{3}c_{4}}{6} + c_{1}q = \frac{2}{3}c_{4}a$$

$$\frac{wa}{3} = \frac{2}{3}c_3a - \frac{2}{3}c_4$$

• Para
$$x_2 = 2a$$
 $x_3 = a$ $y_2 = y_3$

$$\frac{\omega_0}{q}(2a)^3 + \frac{\omega_0^2(2a)^2 - \frac{\omega}{36}(2a)^4 + \frac{2}{3}c_3(2a) + \frac{2}{3}c_4 = \frac{\omega_0}{6}(a)^3 + \frac{c_5(a)}{6}$$

$$\frac{29 \text{ wa}^4 + 463 \text{ a} + 264}{18} = c_5 \cdot \text{a}$$

• Para
$$x_2 = 2a$$
 $x_3 = a$ $y_2' = -y_3'$

$$\frac{\text{Wa}}{3}(2a)^2 + \frac{2}{3}\text{Wa}^2(2a) - \frac{\text{W}}{9}(2a)^3 + \frac{2}{3}c_3 = -\frac{\text{Wa}}{2}(a)^2 + c_5$$

$$\frac{41}{18}$$
 wa $\frac{4}{3}$ c 30 = - c 50.

$$\frac{70}{18}$$
 $\frac{42}{3}$ $\frac{2}{3}$ \frac



$$6wa^4 = 12c_3q - 12c_4$$

 $-70wa^4 = 36c_3q + 12c_4$
 $-64wa^4 = 48c_3q$

$$-\frac{4}{3}wa^3 = c_3$$

$$-\frac{4}{3}wa^{3} = c_{3} \qquad -\frac{11wa^{4}}{6} = c_{4} \qquad -\frac{25wa^{3}}{18} = c_{5}$$

$$-25wa^{3} = c_{5}$$

$$\left| \frac{-25\omega q^3}{18} = c \right|$$

a) deflexion en el centro de la luz

Para
$$x_2 = a$$

$$Tey_2 = \frac{wa}{9}(a)^3 + \frac{wa^2}{3}(a)^2 - \frac{w}{3}(a^4) - \frac{4wa^3}{3}(a) - \frac{11wa^4}{6}$$

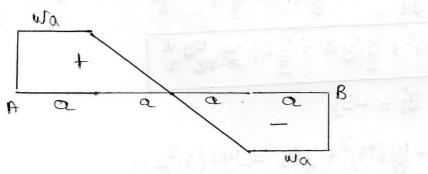
b) Pendiente en A

$$TE\Theta_{A} = C_{1} \quad \Omega_{\Rightarrow} \quad \Theta_{A} = -\frac{25Wq^{3}}{18EI}$$

c) Pendiente en B

IEOB=
$$C_5$$
 $\Omega_{=}$ $O_8 = \frac{-25 w a^3}{18 \in I}$ RATA

9) Ofc



war

E) DMF

REsolver la siguiente viga y determinar el vialor de la daflexión apl el métado de la doble integración, considerar EI=ete.

Tramo
$$0 \le x \le \alpha$$

ETY! = V_{Ax}

ETY! = $V_{Ax}^2 + c_1$

ETY! = $V_{Ax}^2 + c_1$

ETY! = $V_{Ax}^2 + c_1$

ETY! = $V_{Ax}^3 + c_1x + c_2$

ETY! = $V_{Ax}^3 - \frac{(x-\alpha)^3}{6} + c_3x + c_4$

ETY! = $V_{Ax}^3 - \frac{(x-\alpha)^3}{6} + c_3x + c_4$

ETY'' =
$$\sqrt{4}x^2 - \sqrt{6}(x-30) - \rho(x-20)$$

ETY'' = $\frac{\sqrt{4}x^2}{2} - \frac{\sqrt{4}}{2}(x-30)^2 - \frac{\rho(x-20)^2 + c_5}{2}$
ETY'' = $\frac{\sqrt{4}x^3}{6} - \frac{\sqrt{4}}{6}(x-30)^3 - \frac{\rho(x-20)^3 + c_5x + c_6}{2}$

$$\sqrt{1^{EQA}}$$
 ef X=0 y=0 → C₂=0
 $\sqrt{1^{EQA}}$ ec X=a y'=y'₂ → C₁= C₃
 $\sqrt{2^{CA}}$ ec X=a y₁=y₂ → C₂= C₄
 $\sqrt{2^{CA}}$ ef X=3a y'₃=0

$$0 = \sqrt{A}(3a)^{2} - \frac{\omega a}{2}(3a - 3a)^{2} - \frac{P}{2}(3a - 2a)^{2} + C5$$

$$0 = 9a^{2}NA - 9a^{3}\omega - \frac{Pa^{2}}{2} + C5$$

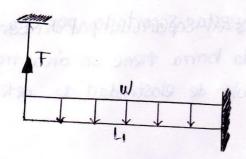
$$C5 = 9a^{3}\omega + \frac{Pa^{2}}{2} - \frac{9a^{2}Na}{2}$$

 $\frac{\sqrt{A}(2a)^{3}}{24}(2a-a)^{4} + c_{3}(2a) = \frac{\sqrt{A}(2a)^{3}}{24} = \frac{\sqrt{A}(2a-\frac{3}{2}a)^{3}}{24} - \frac{P(2a-2a)^{2}}{24} + c_{5} \times + c_{6}$ 10 0+ 140 0 - 10 0 W - 180 W + 45 W04 + 4 Pa = 9 VA 03 $\frac{23}{6}q^{4}w + \frac{4}{3}Pa^{3} = 9VAa^{3} VA = \frac{23}{70}aw + \frac{4}{27}P$

$$V_B = \frac{49 \text{ Wa} + 23 \text{ P}}{72}$$

$$MA = \frac{13\sqrt{a^2 + 5}Pa}{24}$$

doble Integración



$$TEY' = Fx - \frac{\omega x^2}{2}$$

$$TEY' = \frac{Fx^2}{2} - \frac{\omega x^3 + c_1}{6}$$

$$TEY = \frac{Fx^3}{6} - \frac{\omega x^4 + c_1x + c_2}{24}$$

Para
$$x=L_1$$
 $y'=0$ Pora $x=L_1$ $y=0$

$$0 = \frac{F}{2} (L_1)^2 - \frac{\omega}{6} (L_3) + Q$$

$$C_1 = \frac{\omega L_1^3}{6} - \frac{7}{2} L_1^2$$

$$C_2 = \frac{7}{3} \frac{\omega L_1^4}{8}$$

$$0 = \frac{7}{2}(L_1)^2 - \frac{\omega}{6}(L_1^3) + C_1$$

$$0 = \frac{7}{6}(L_1^3) + \frac{\omega}{6}(L_1^3) + \frac{\omega}{6}$$

$$c_2 = \frac{Fl_1^3}{3} - \frac{\omega l_1^4}{8}$$

$$fora x = 0$$

$$EIY = C_2 = \frac{1}{3} - \frac{3}{8} = \frac{3}{8} = \frac{3}{8} = \frac{3}{3}$$

$$y = \frac{\omega L_1^4}{8 \epsilon I} - \frac{F L_1^3}{3 \epsilon I} \left(\frac{1}{4} \right)$$

$$d = FL = \frac{WL'^4}{8EI} = \frac{TL^3}{3EI}$$

$$F = \frac{3W E_{2} A_{2} L_{1}^{4}}{8(3 \epsilon_{1} L_{1} L_{2} + E_{2} A_{2} L_{1}^{3})}$$

Pota